

# Determining key parameters and suitable measures for successful EGS developments

David Bruhn

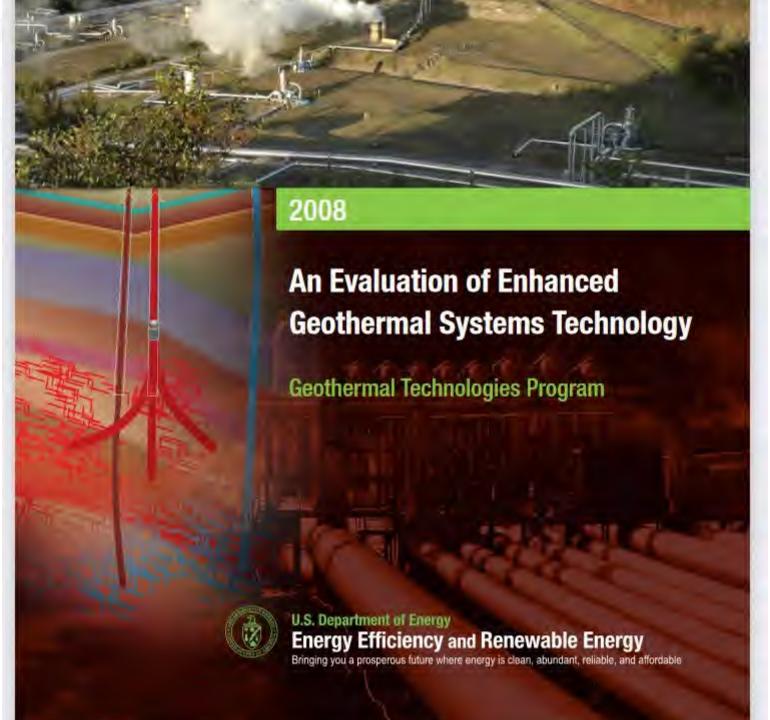
TU Delft
Dept. of Geoscience & Engineering



GFZ Potsdam Section Geoenergy



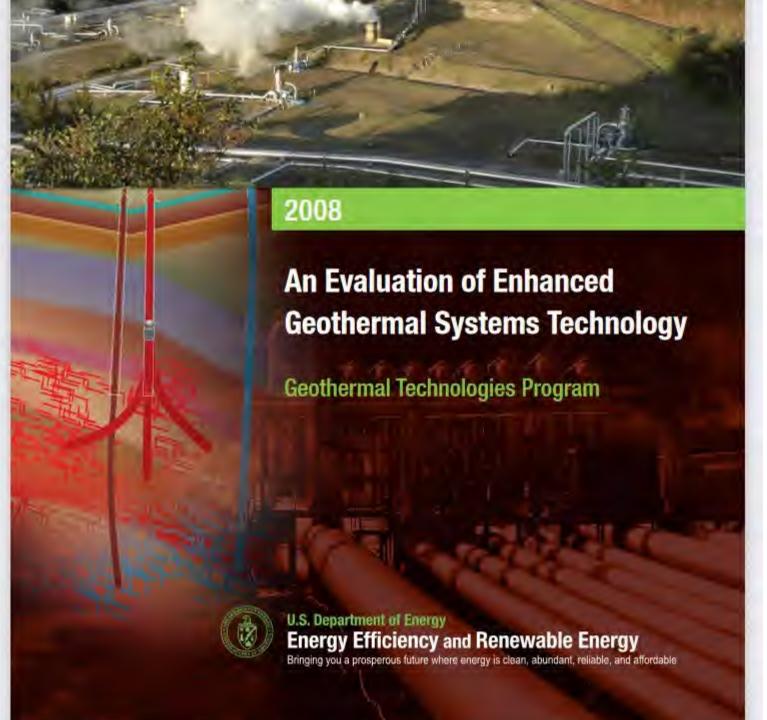














# **Key Components**

Various site properties that should be known for successful creation of the reservoir include

- Temperature gradient and heat flow
- Stress field
- Lithology and stratigraphy
- Structure and faulting
- In situ fluids and geochemistry
- Geologic history
- Seismic activity
- Proximity to transmission
- Land availability
- Demographics



# Fenton Hill - First HDR Project

1974-1992

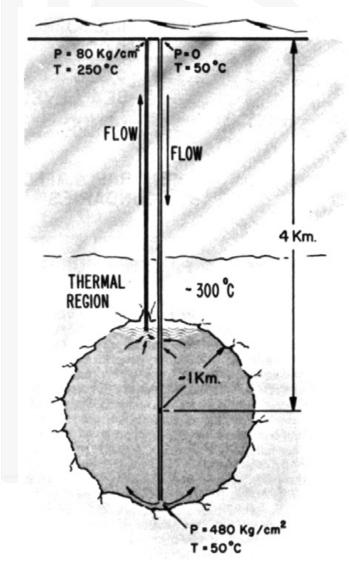




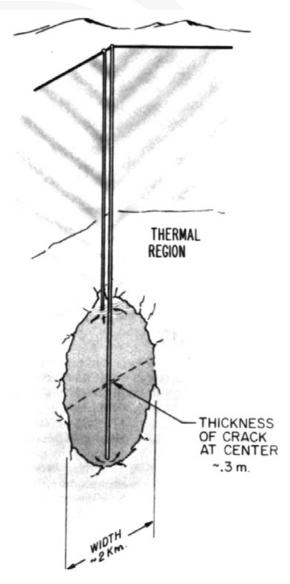


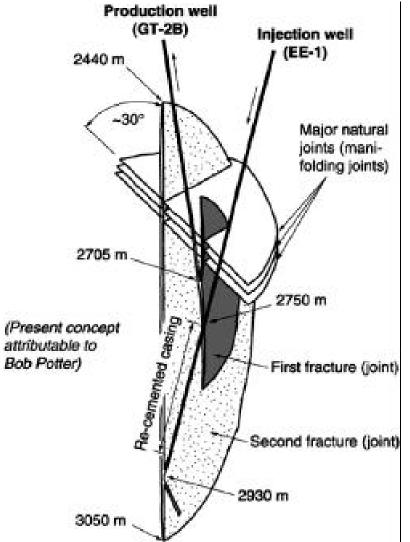


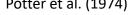


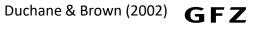


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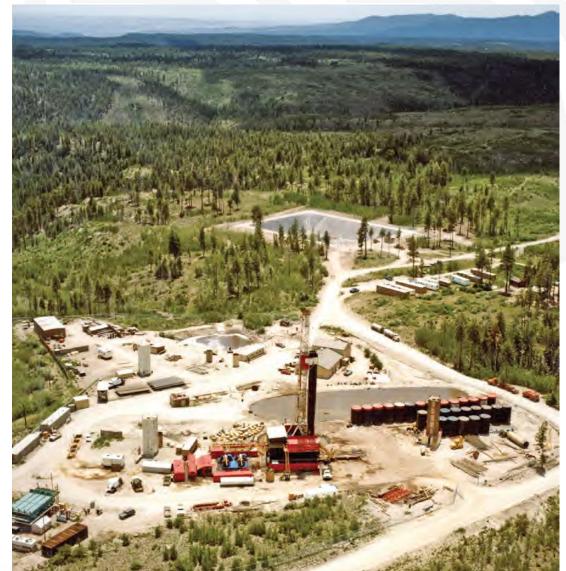


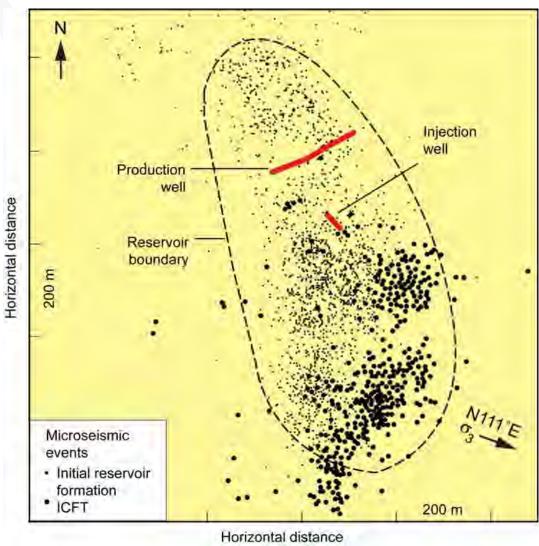


# Fenton Hill - First HDR Project



1974-1992









# Some Lessons Learnt from Fenton Hill



- Deep (~5 km), high-temperature wells can be completed in hard, abrasive rock
- Low-permeability crystalline rock can be stimulated to create hydraulically conductive fractures.
- Hydraulic-pressurization methods can create permanently open networks of fractures in large enough volumes of rock (>1 km3) to sustain energy extraction over a long time period.
- The EGS reservoir can be circulated for extended time periods and used to generate electricity.
- Creating the connection between wells was a crucial step in developing the EGS reservoir.
   Connection was easier to establish by drilling into the fractured volume, once it was stimulated and mapped.
- The fracture pattern that was observed did not match that predicted by early modeling.
- If water was injected at high enough pressures to maintain high flow rates, the reservoir grew and water losses were high. If injection pressures were lowered to reduce water loss and reservoir growth, the flow rates were lower than desired, due to higher pressure drop through the reservoir
- The high pressures needed to keep the joints open caused operational problems and required substantial amounts of power.



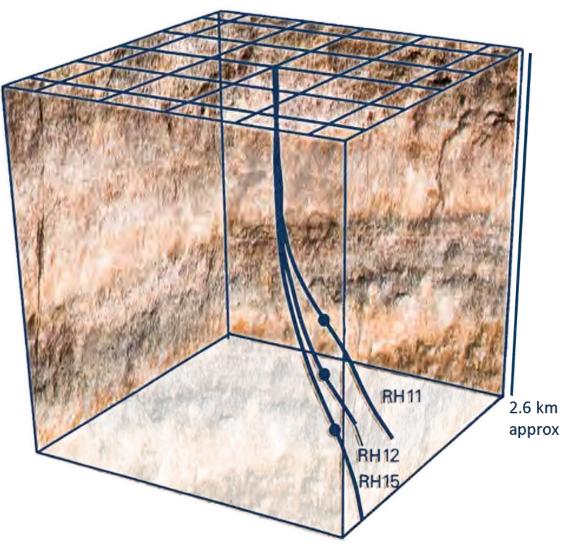


# Rosemanowes, UK

1977-1991

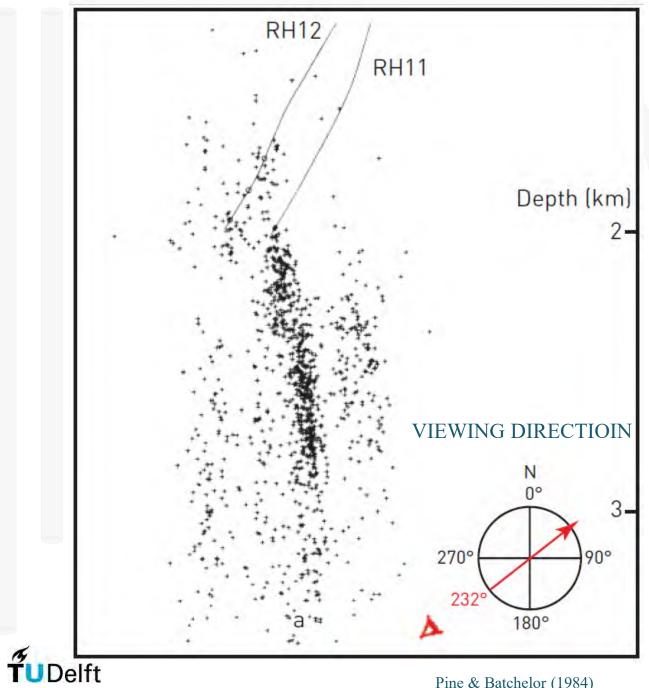






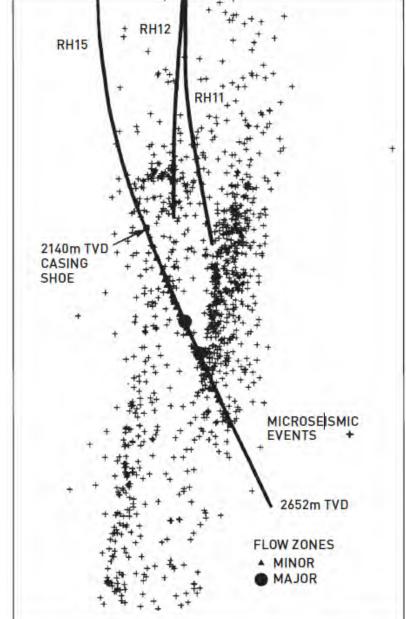














## Lessons Learnt from Rosemanowes



- The fractures created by hydraulic stimulation, which best connect across the reservoir, are not formed through tension. Instead, they are created by shearing on pre-existing joint sets.
- Stress fields in crystalline rock are invariably anisotropic, so the natural fractures fail in shear. Having sheared, the natural fractures then self-prop and stay open.
- It is possible to stimulate natural fractures and improve permeability and create a connected volume of hot rock.
- A prediction of the direction of fracture growth is difficult in the absence of precise downhole data. Even with near-wellbore data from image logs, the fractures may not grow exactly as predicted. As a result, it is better to create the reservoir first, and then drill into it (Batchelor, 1987).
- Probably the most important single lesson from this experiment is that hydro-fracturing and artificial fractures are almost irrelevant. The natural fracture system dominates everything (Batchelor, 1989).
- Overstimulating pre-existing fractures can result in a more direct connection from injector to producer than is desired, so that cool fluid can "short-circuit" through the reservoir.

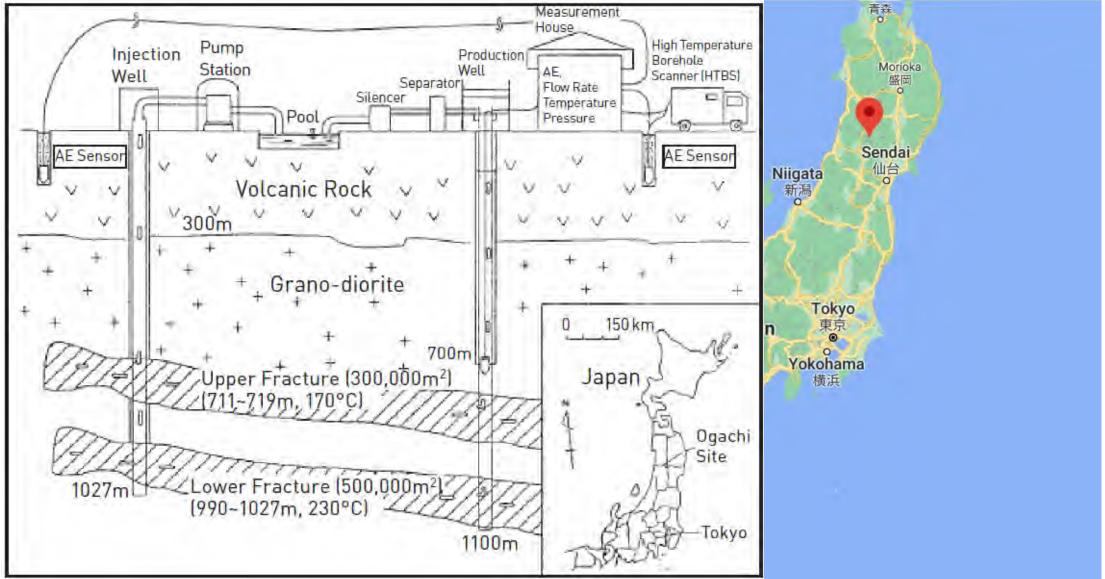




# Ogachi and Hijori, Japan

1989-2002









# Lessons Learnt from Hijori



- The reservoir continued to grow during the circulation test.
- If natural fractures already connect the wellbores, stimulation may result in an improved connection that causes short circuiting, particularly if the well spacing is small.
- The acoustic emissions (AE) locations from the deep circulation test suggest that the stimulated fractures or the stress field change direction away from the well.

# Lessons Learnt from Ogachi

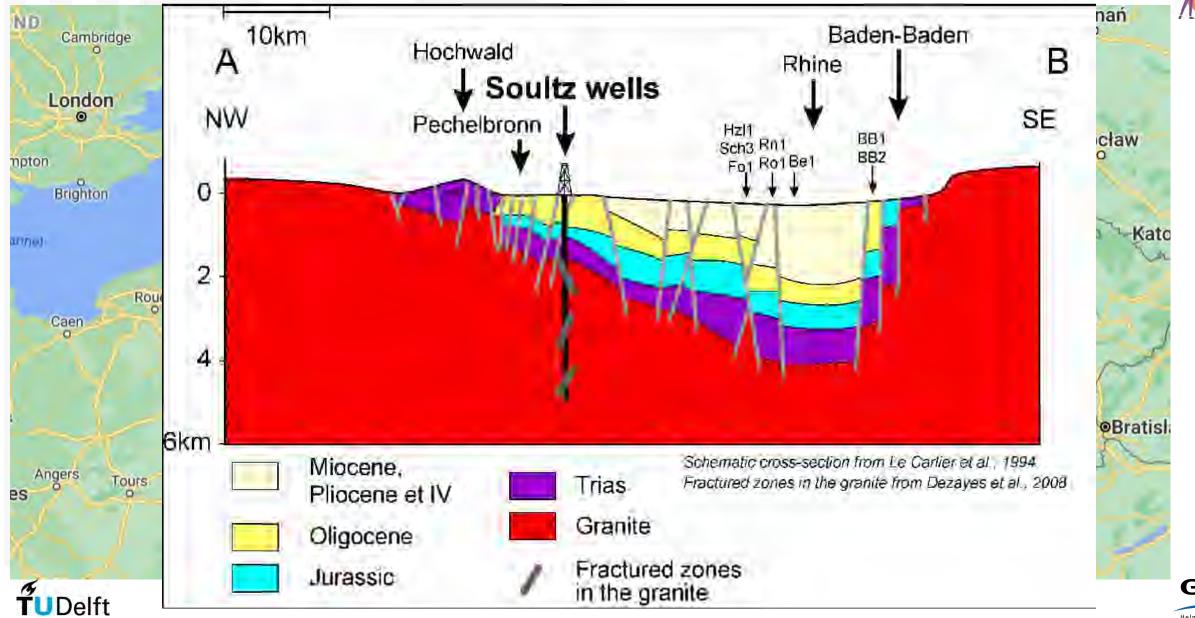
- The complex geologic history at Ogachi made it difficult to predict the direction of fracture growth.
- The stress state in the original boreholes was not well understood until borehole televiewer data was collected and analyzed after the wells had been stimulated.
- Stress changes with depth in the boreholes





1987-





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### The European EGS test site Soultz-sous-Forêts, France



Objective 2 x 1.5 MW electrical power (1.5

MW capacity currently installed)

Wells 3

Vertical Depth 5.000 m

**Temperature** > 180°C

Flow Rate  $2 \times 125 \text{ m}^3/\text{h}$ 

**Reservoir** EGS/HDR/petrothermal

Power Plant ORC

**Research** 1987 to 2005

**Construction** 2005 to 2008

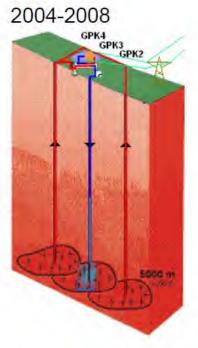
**Status** feed-in of up to 1.5 MWe

- target horizon 5000 m
- temperature 200°C
- 35 l/s → 2.0 MWe (well distance 600 m)







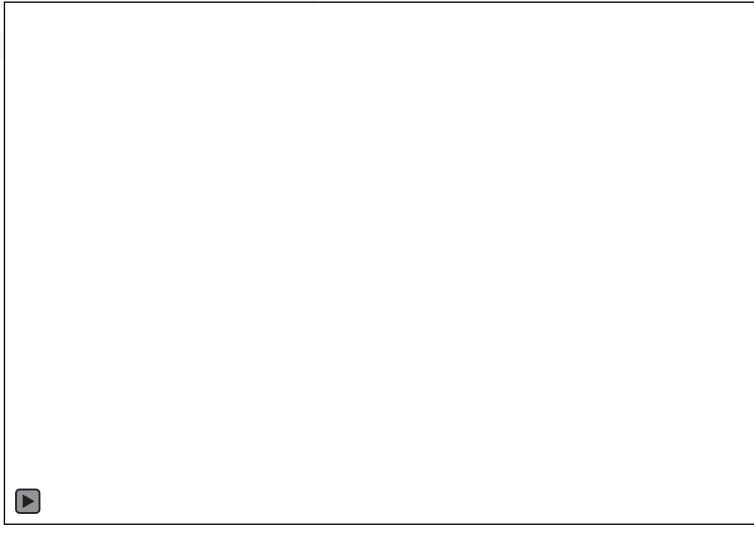






# Monitoring fracture growth





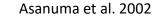




# Monitoring fracture growth







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### The European EGS test site Soultz-sous-Forêts, France



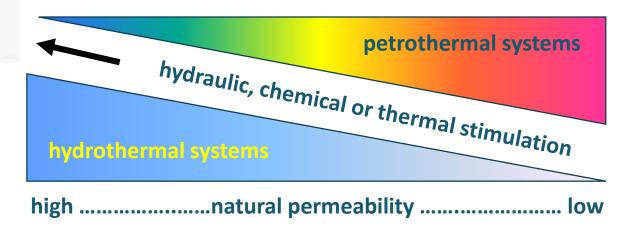
- 22 years of research, from first site investigation to operation and electricity production in 2008
- 80 MEuros spent on RTD and installations: 30 M€ EU, 25 M€ France, 25 M€ Germany.
- The initial French-German cooperation was enlarged by adding the UK experience (Camborne School of Mines -> Rosemanowes)
- 15 research institutions and numerous subcontractors involved
- More than 40 PhD theses, 1000+ scientific publications
- Regional spin-offs in Landau, Insheim, Bruchsal, Rittershoffen, Strasbourg ...
- Now operated by ES Géothermie

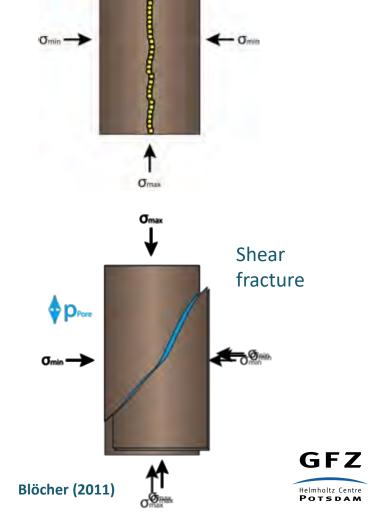




# Enhanced geothermal systems (EGS)

- The EGS concept: artificial improvement of hydraulic performance of a reservoir
- Enhancement is required to develop and exploit geothermal resources that are not economically viable by conventional methods
- Enhanced vs Engineered





Piny

Geothermal Winter School 2021

Extensional

fracture



# Geology - fractures



### **Properties**

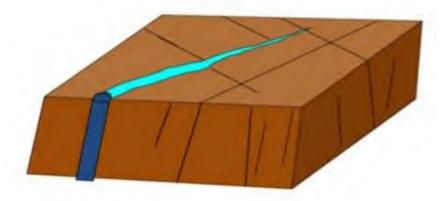
- Fracture sets
- Fracture intensity
- Fracture orientation
- Fracture size
- Fracture conductivity
- Mechanical properties

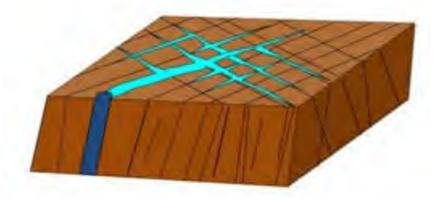
### **Exploration**

- Well logs (e.g. FMI, PLT,...)
- Seismics (active, passive)
- Production data & well tests
- Outcrop studies

### **Implications**

- Hydro-shearing of critically stressed preexisting fractures
- Interaction with existing fractures
- Locally fracture follows fabric





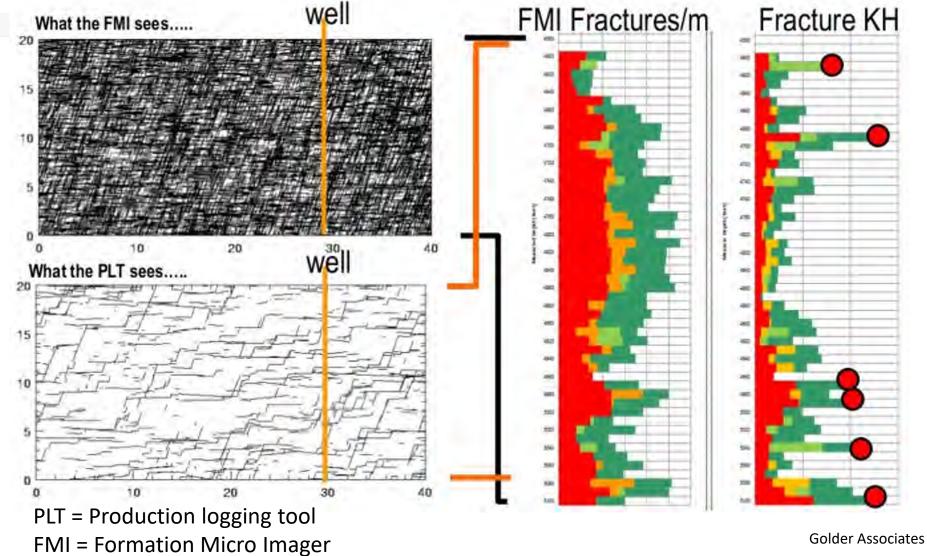
McLennan and Potocki (2013)





# Geology – fractures from well logs





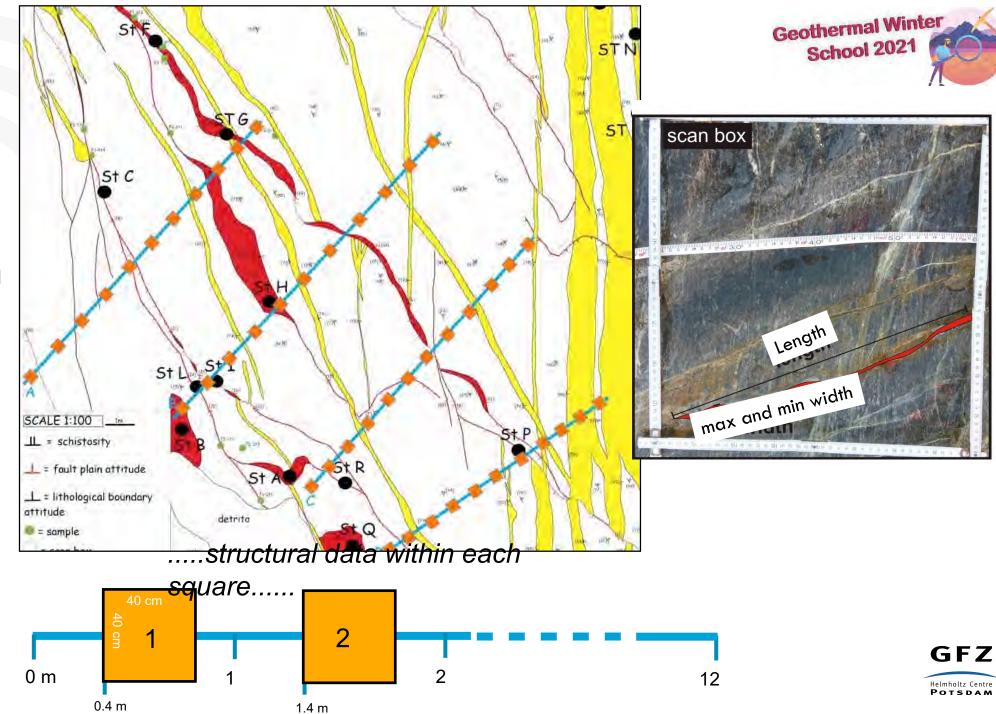




# **EXERCISE**

Fracture mapping: Scanlines from analogue sites

**T**UDelft



**EXERCISE** 



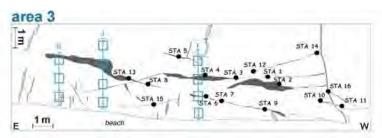


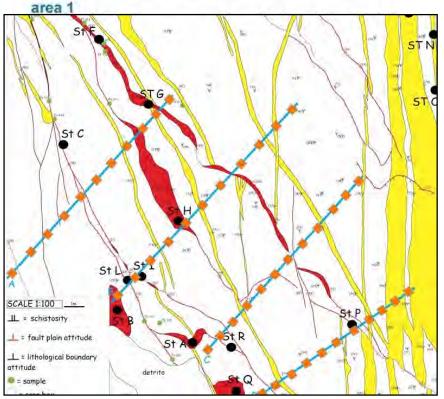
area 2





### .....TOWARDS PERMEABILITY.....









### **PARAMETERS**

### PERMEABILITY (m<sup>2</sup>)



$$k = \left(\frac{2}{3} \times \frac{b^3}{L}\right) \times \left(f \times 10^{-6}\right)$$

Gale (1982)

Nicholl et al. (1999)

Zimmerman and Bodvarsson, 1996

b = average fracture width L = fracture length

f = assumed as 0.4

Connectivity among fractures 0.1 < f < 1

*f* = constant of connectivity







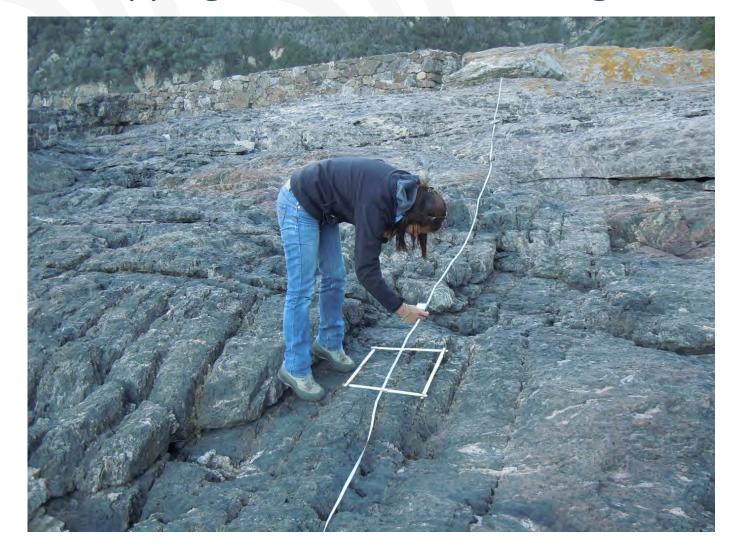




# **EXERCISE**



# Fracture mapping: Scanlines from analogue sites







# **EXERCISE**

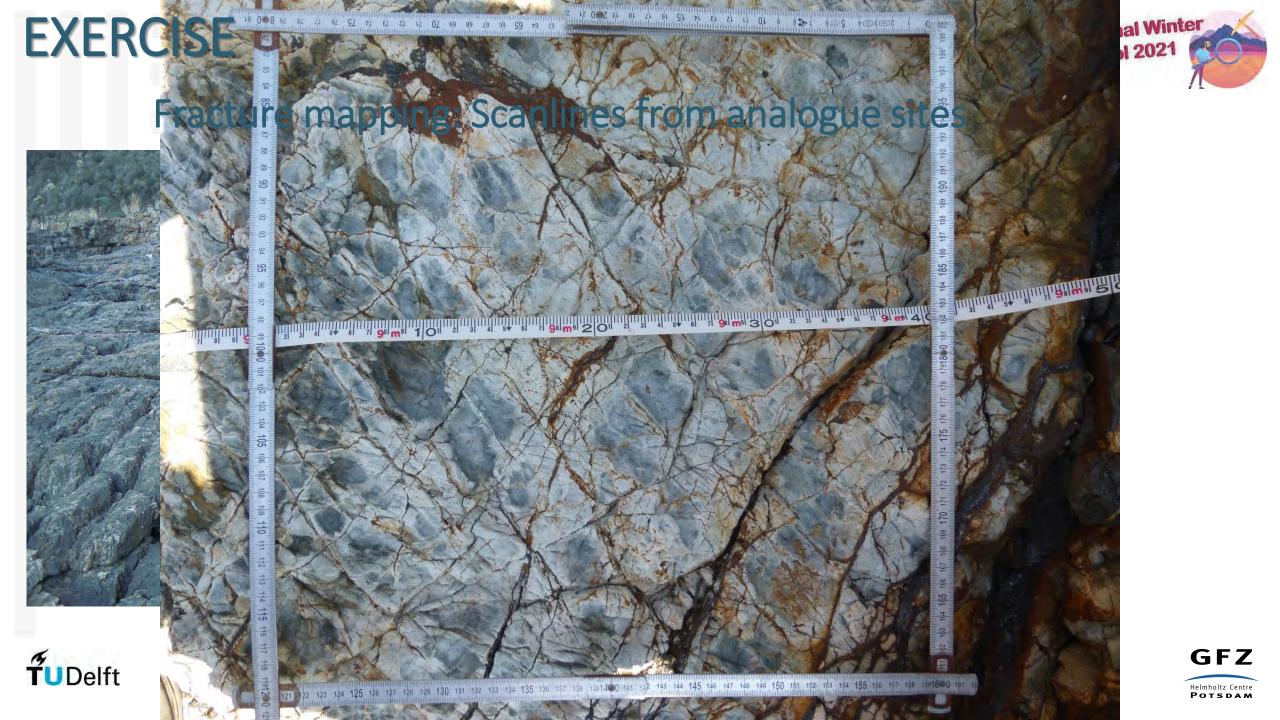












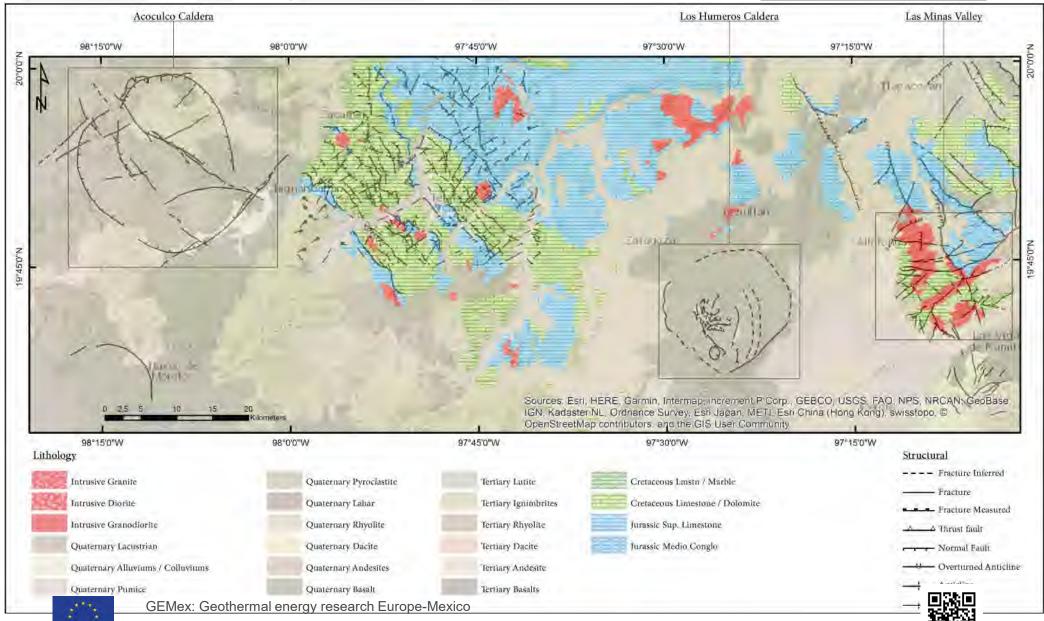








### Las Minas analogue site







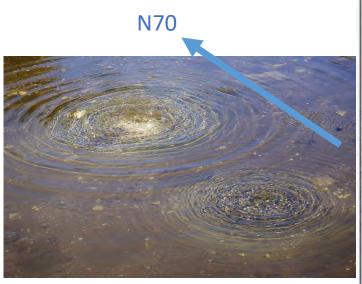
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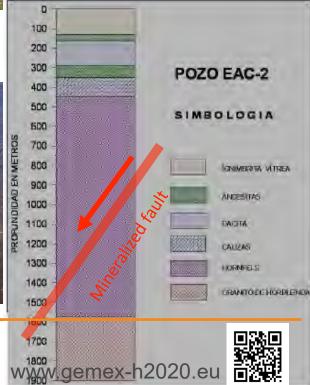
ol 202°

### Acoculco













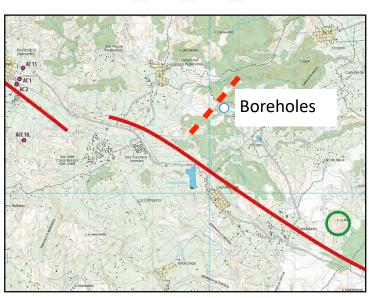


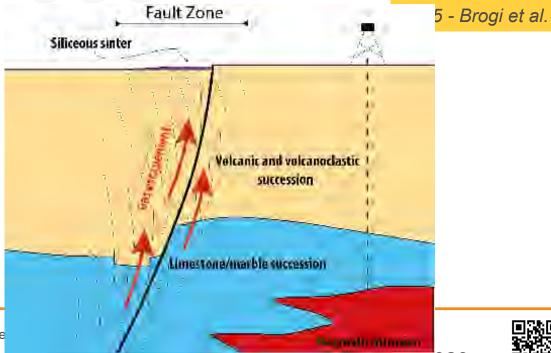
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# Mapping at Acoculco











GEMex: Geothermal energy research Europe



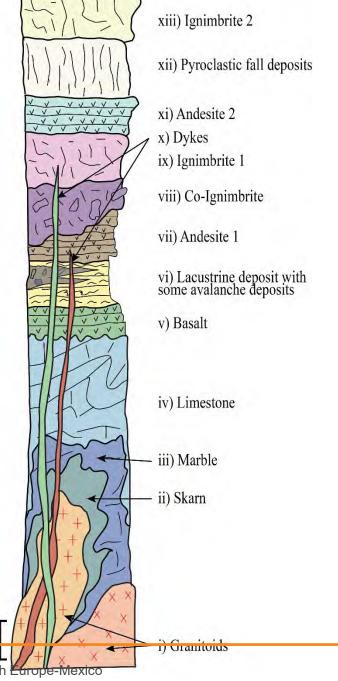


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# Lithological Units Las Minas

Analogue site for Accoculco and Los Humeros







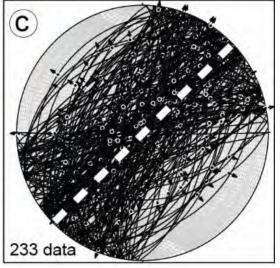




nal Winter

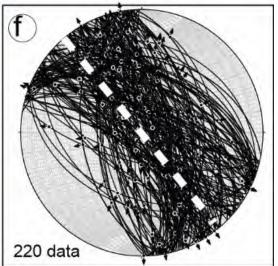


















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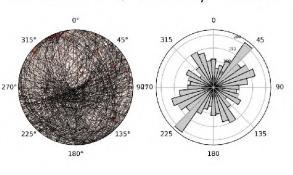
GFZ

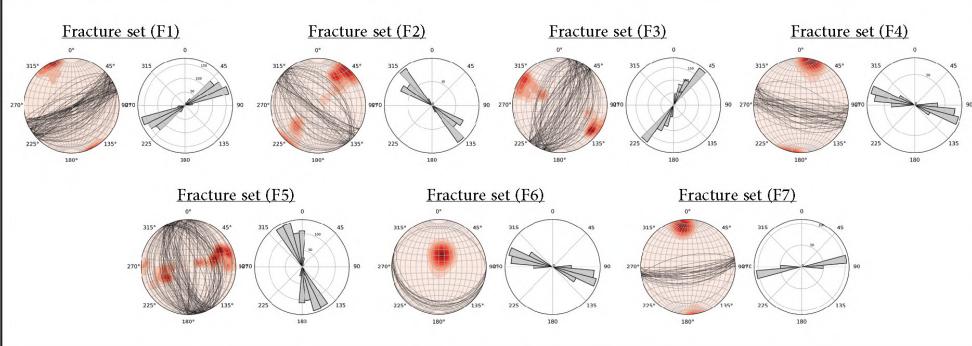
Helmholtz Centre
Potsbam



### Las Minas Stereographic projection plots

All fracture sets, from every scanlines









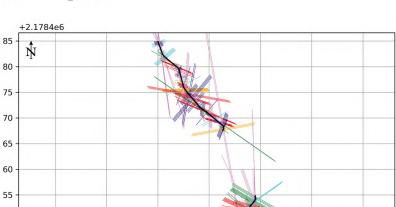


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### Fracture mapping: Scanlines from analogue sites



Boquillas



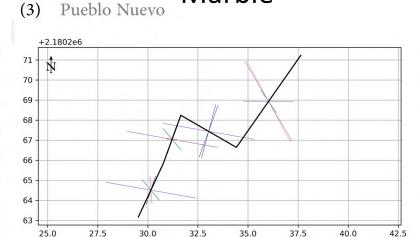
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694490

694500

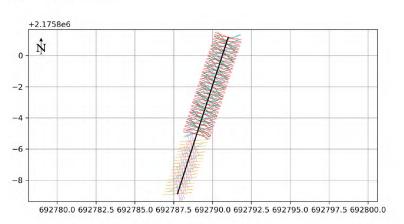
Skarn

Marble



Rinconada

+6.93e5

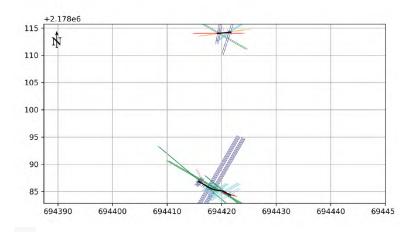


Eldorado

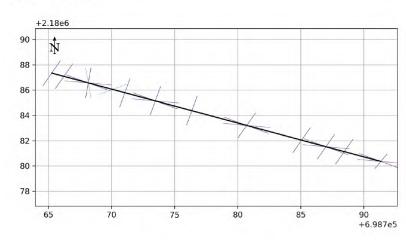
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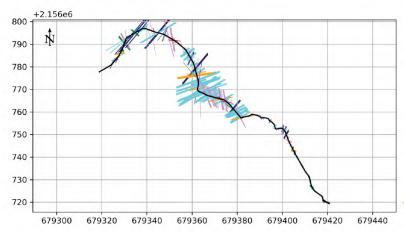
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Tatatila



San Antonio Tenextepec



Lepillier (2020)





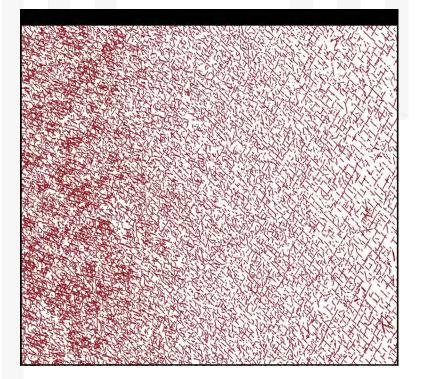




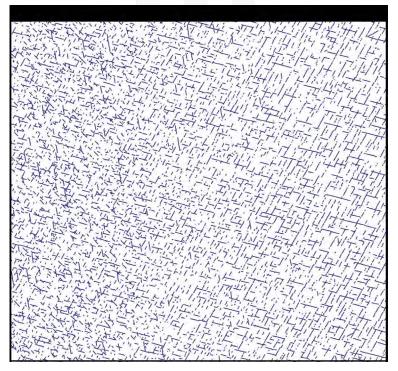
### Computed DFNs using the MPS method



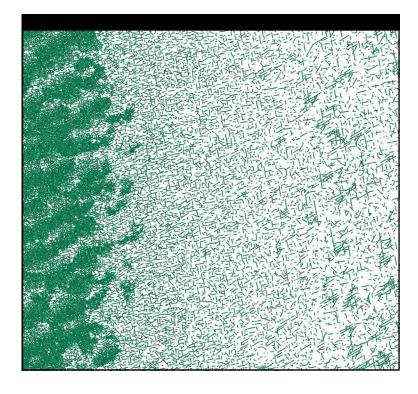




Marble



Limestone





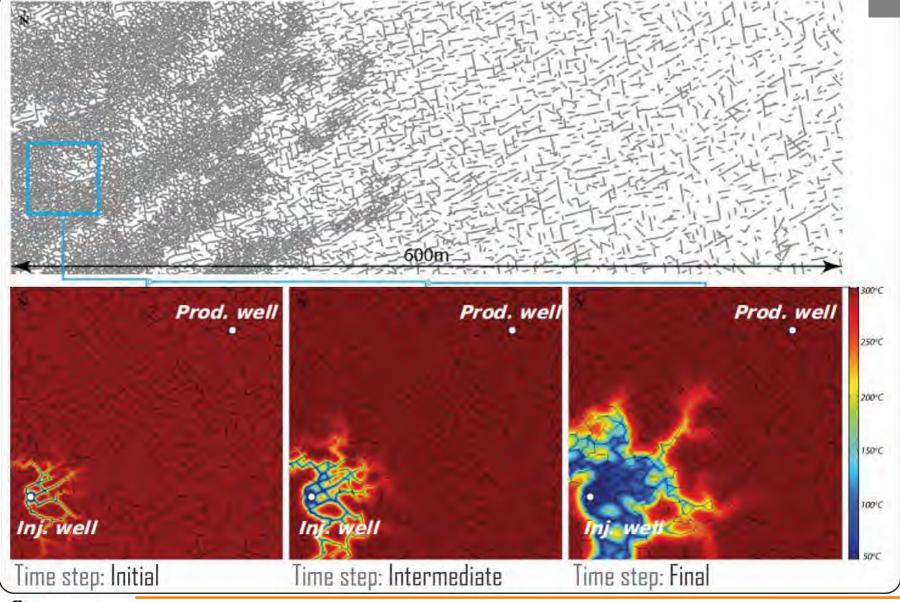








### Fracture controlled fluid flow simulation









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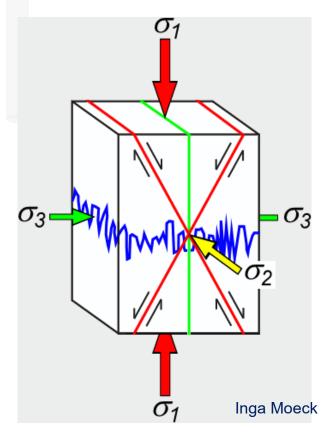




### Fractures as result of forces

- Stress and forces in 3 main axes
- material: fracture strength, shear strength
- characteristic angle +/- 30° from max. main stress direction to shearing



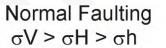


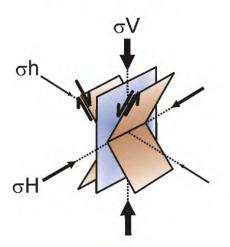




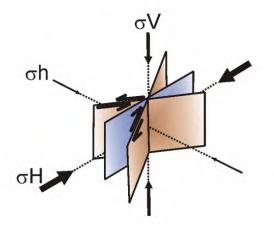
# Stress Regimes



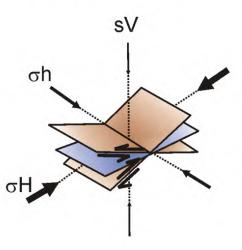


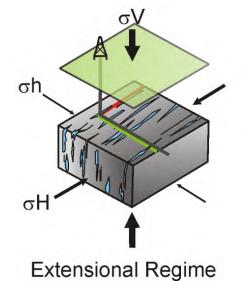


Strike-slip Faulting  $\sigma H > \sigma V > \sigma h$ 

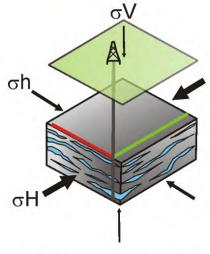


Reverse Faulting  $\sigma H > \sigma h > \sigma V$ 





σh
σH
Strike-slip Regime

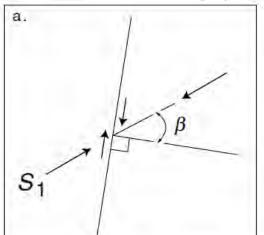


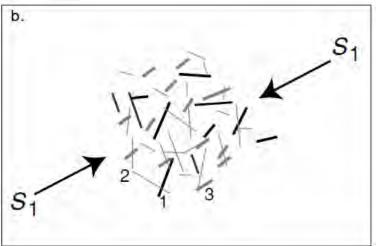


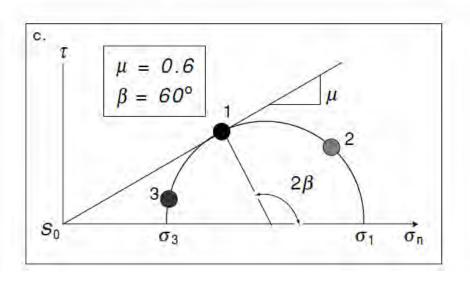










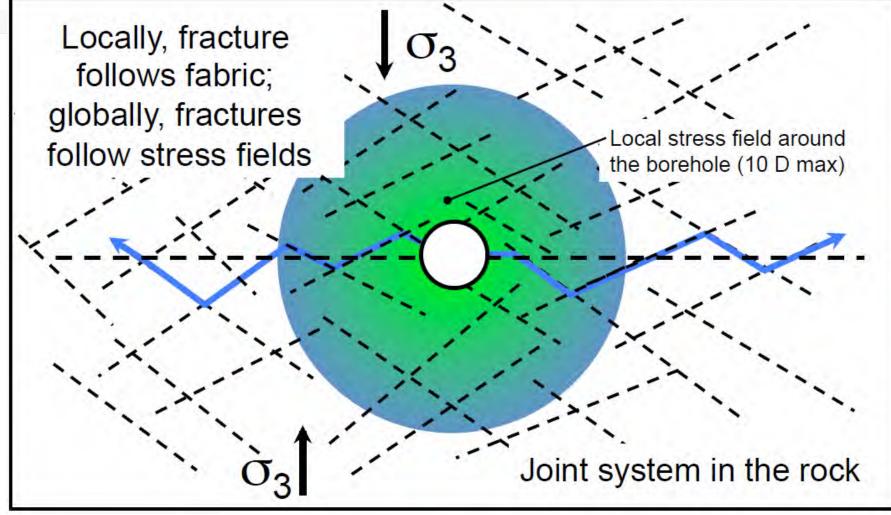






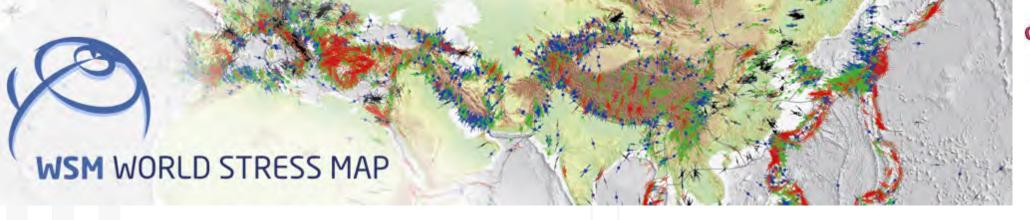
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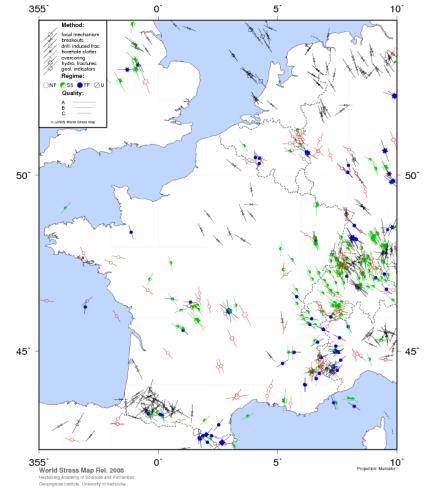


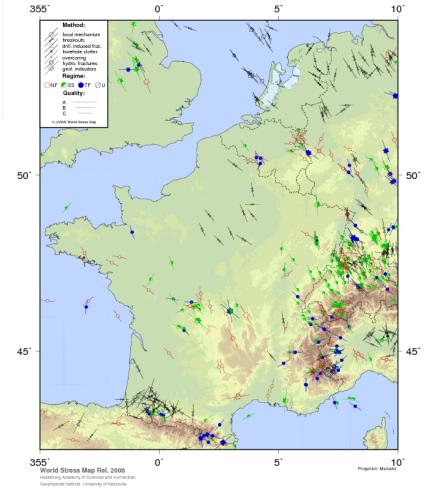






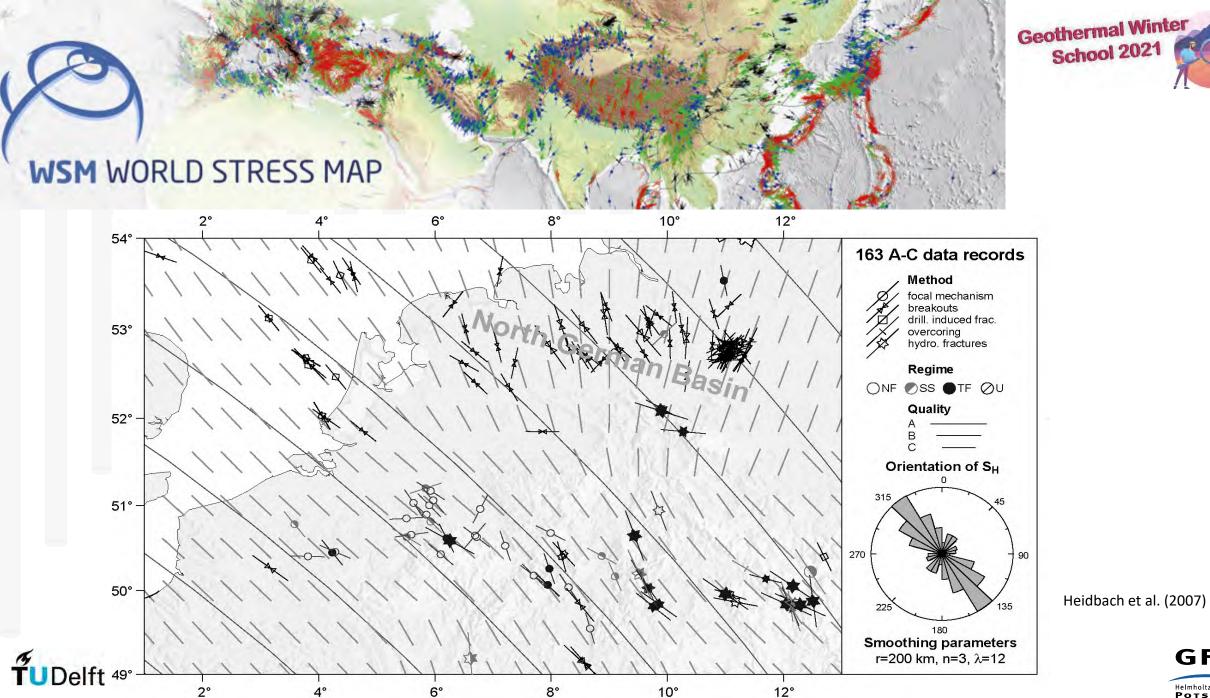






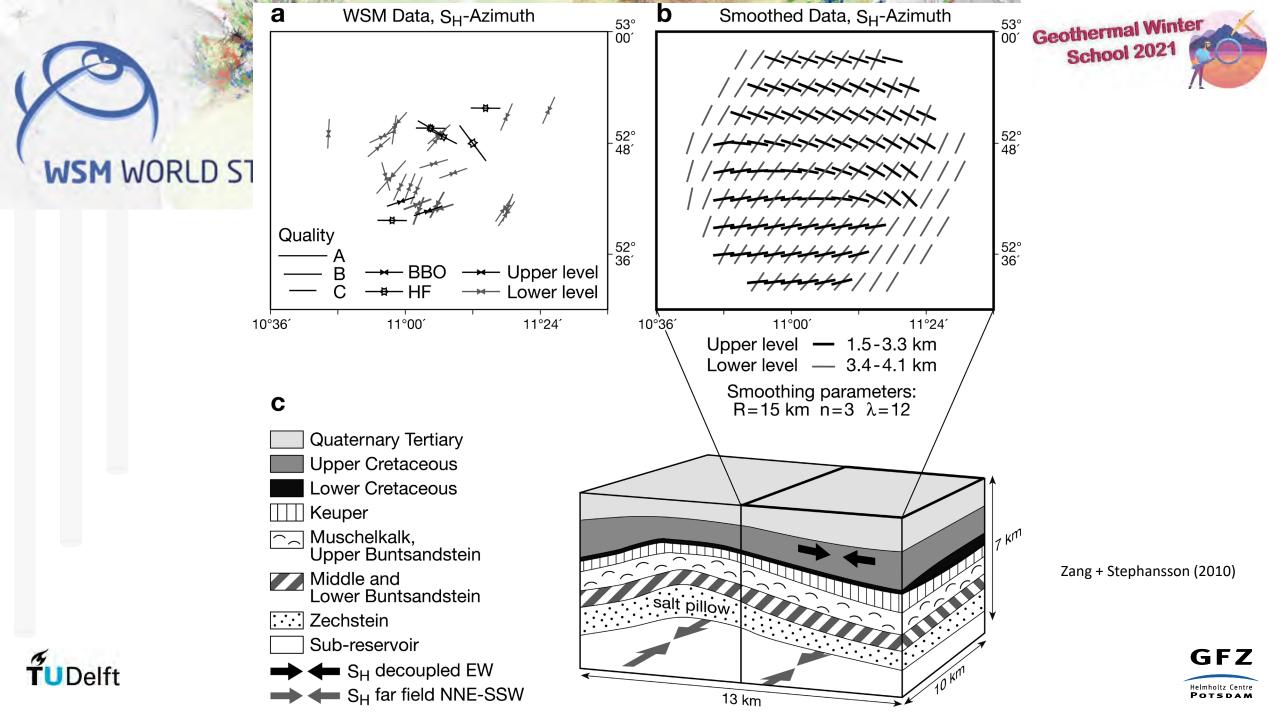




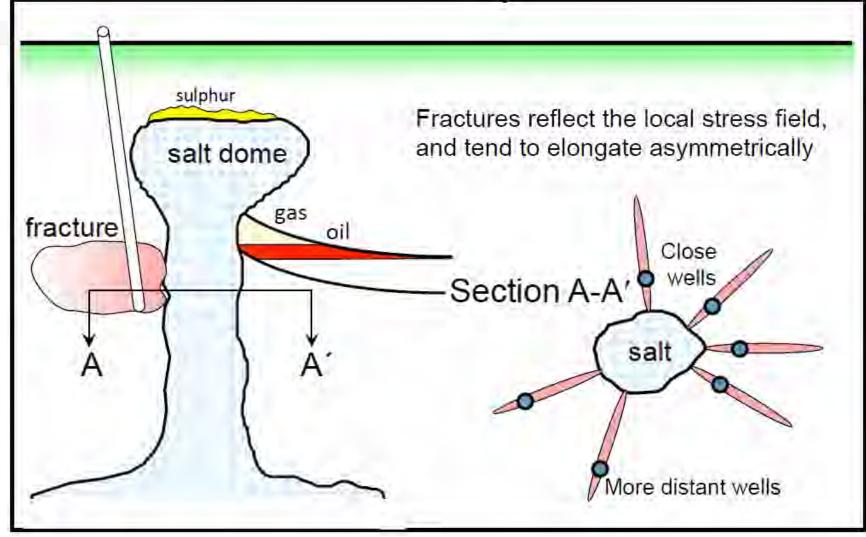












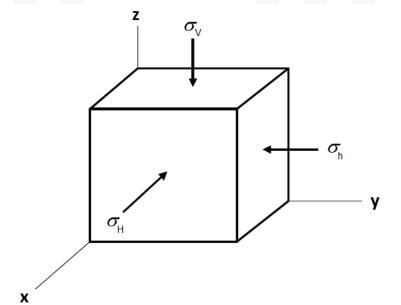
Dusseault





### **Properties**

- Stress magnitudes
- Stress directions
- Stress gradients
- Pressure



#### **Exploration**

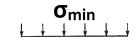
- SV: Density log
- Sh: Minifrac/LOT
- **Orientations:** 
  - **Breakouts**
  - Tensile fractures
  - HF orientations
  - Focal mechanisms
  - Shear velocity anisotropy
  - Geological indicators
- SH: constrained based on the parameters above
- P: direct measurement

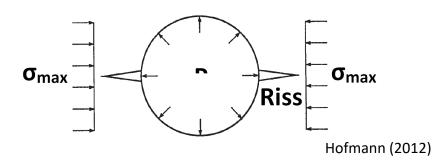
#### <u>Implications</u>

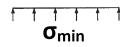
Fracture growth directions

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- Containment
- Critical pressures for fracture opening/ shearing/closure
- Active/inactive faults
- Shear failure potential





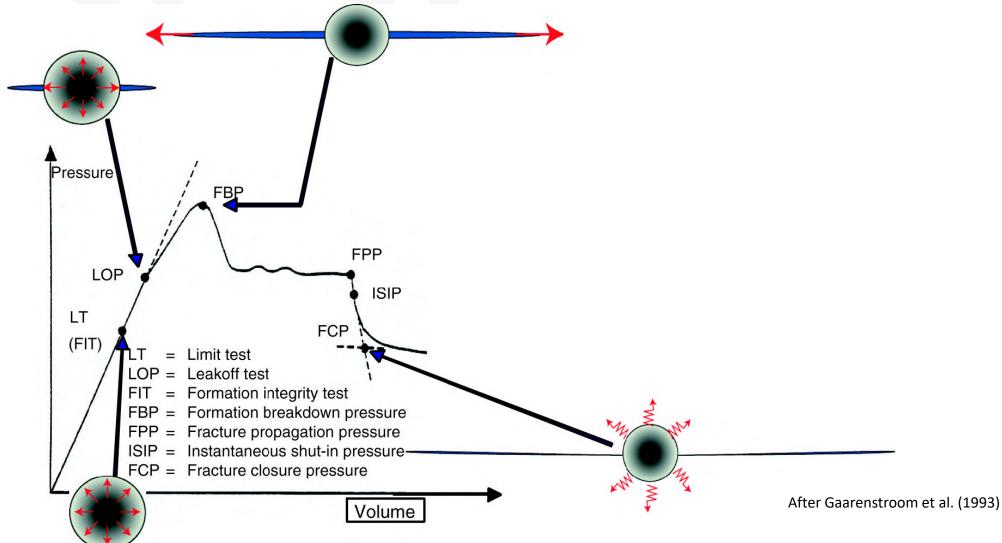






### Stress field - downhole

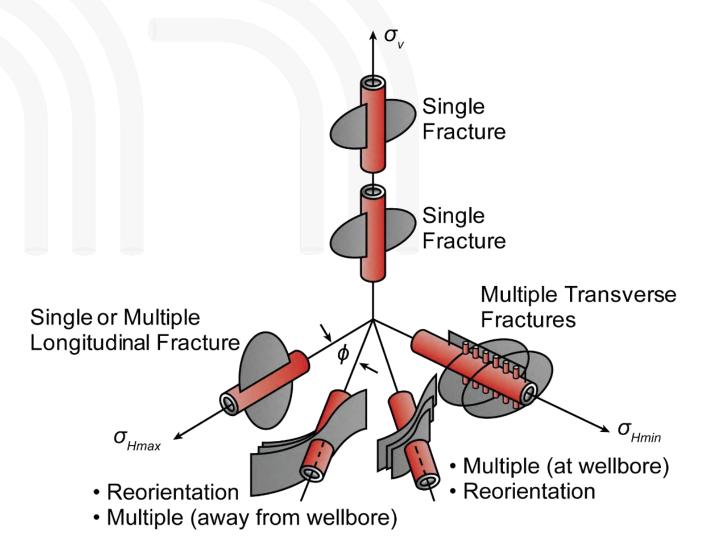














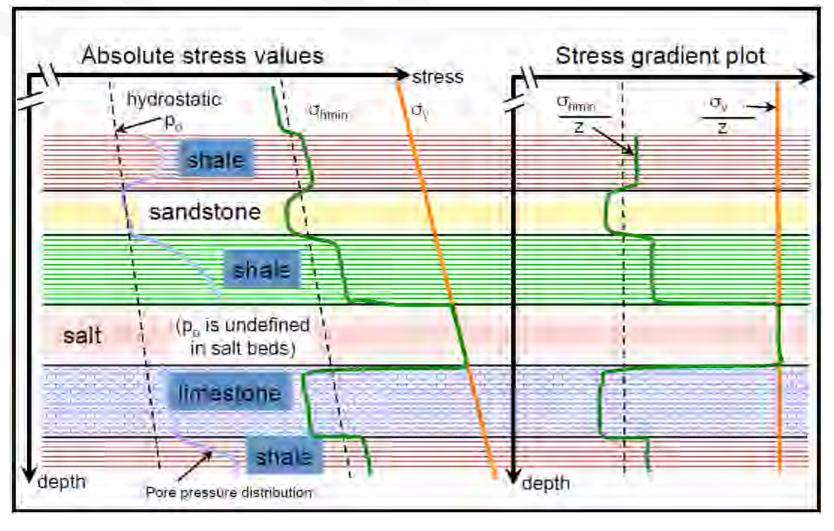




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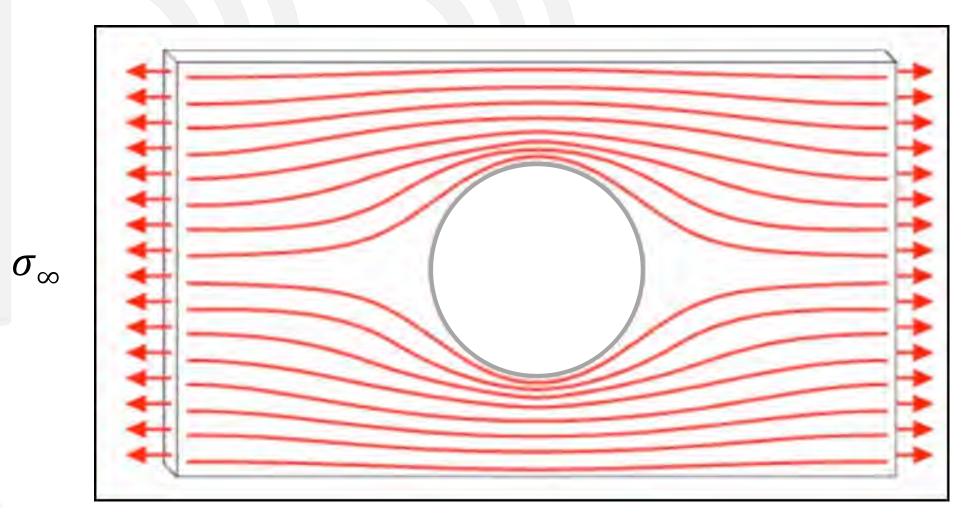




# **EXERCISE**



### Stress Concentration Around Borehole









### **EXERCISE**



# Wellbore Fracture Initiation: Impermeable Borehole Wall, $\sigma_h \neq \sigma_H$

$$p_w^{frac} = 3\sigma_h - \sigma_H - p + T_0$$

For the isotropic stress case  $\sigma_h = \sigma_H$ simply replace  $3\sigma_h - \sigma_H$  with  $2\sigma_h$ 

$$p_w^{frac} = 2\sigma_h - p + T_0$$







## Pore pressure vs. stress

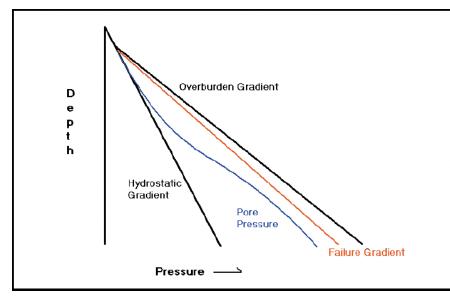
pore pressure
vertical stress (overburden)
mean stress
effective stress (Terzaghi, 1936)

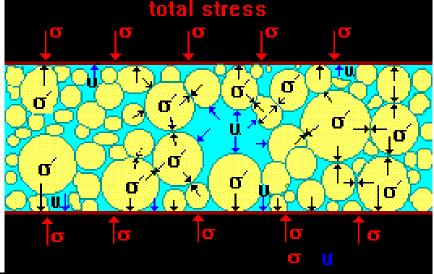
$$p = \rho gh + p_0$$

$$\sigma_V = \rho_s gh$$

$$\sigma = (\sigma_V + \sigma_H + \sigma_h)/3$$

$$\sigma_{eff} = \sigma - p$$

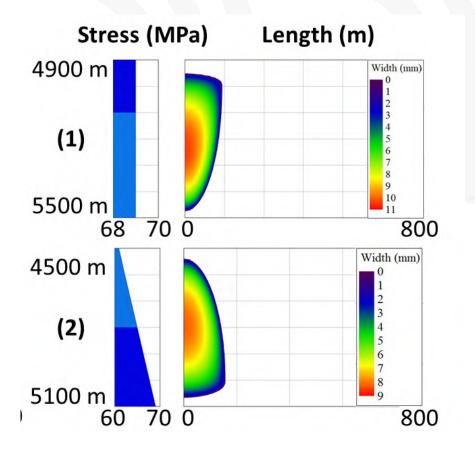


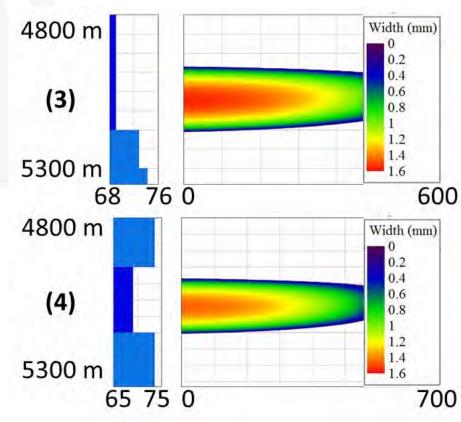




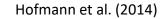








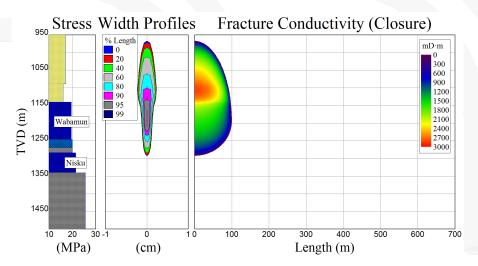


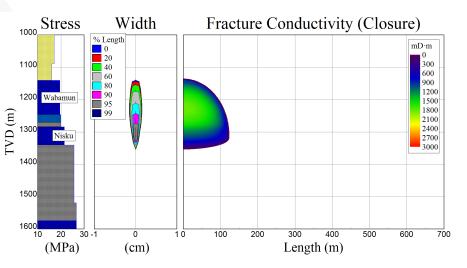


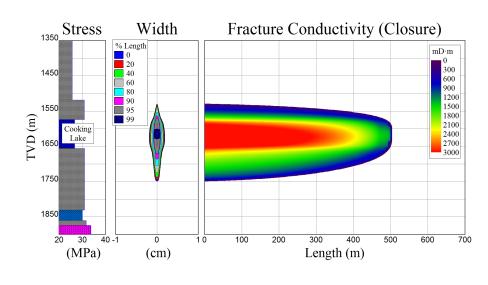


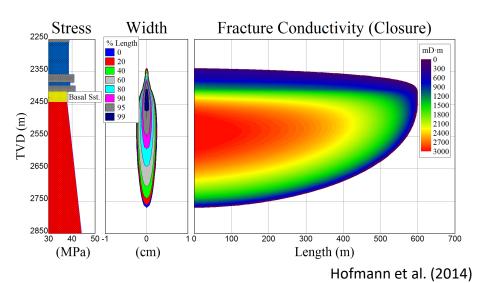
# Geology - Stratigraphy















# Rock properties - hydraulic



#### **Properties**

- Permeability
- Porosity
- Which fractures are conductive

#### **Exploration**

- Well logs
- Well tests
- Core samples
- Production data

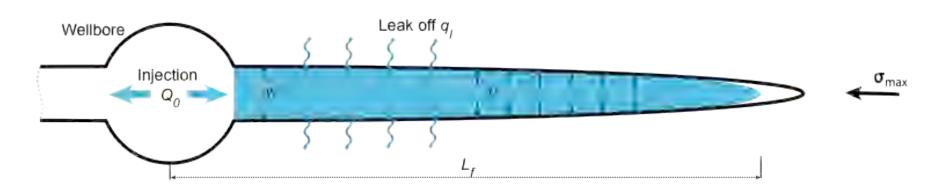
#### **Implications**

- Fluid leak-off
- Fluid loss
- Frac fluid volume
- Zonal isolations
- Leak-off barriers

#### Mass balance:

$$V_i = V_{Lp} + V_f$$



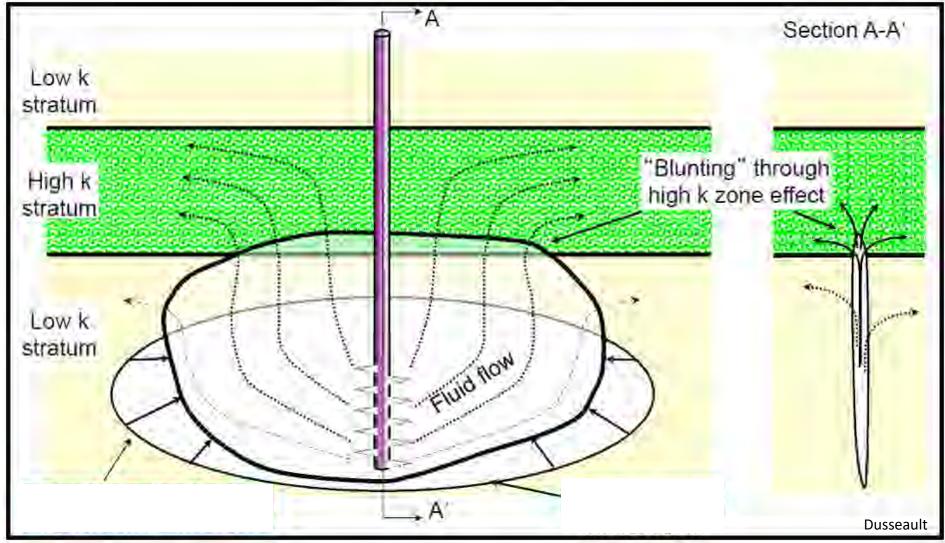






# Rock properties - hydraulic









# Rock properties - mechanical



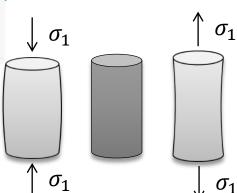
#### **Properties**

- Young's modulus
- UCS
- Tensile strength
- Cohesion
- Friction angle

#### uniaxial

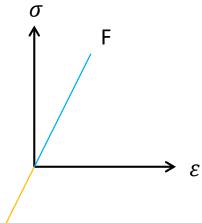
extension

#### compression



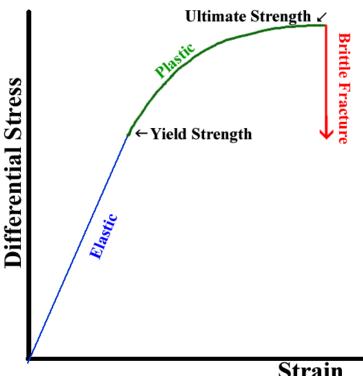
#### **Exploration**

- Core samples (lab tests)
- Well logs



#### **Implications**

- Fracture aperture
- Self-propping
- Fracture mechanics





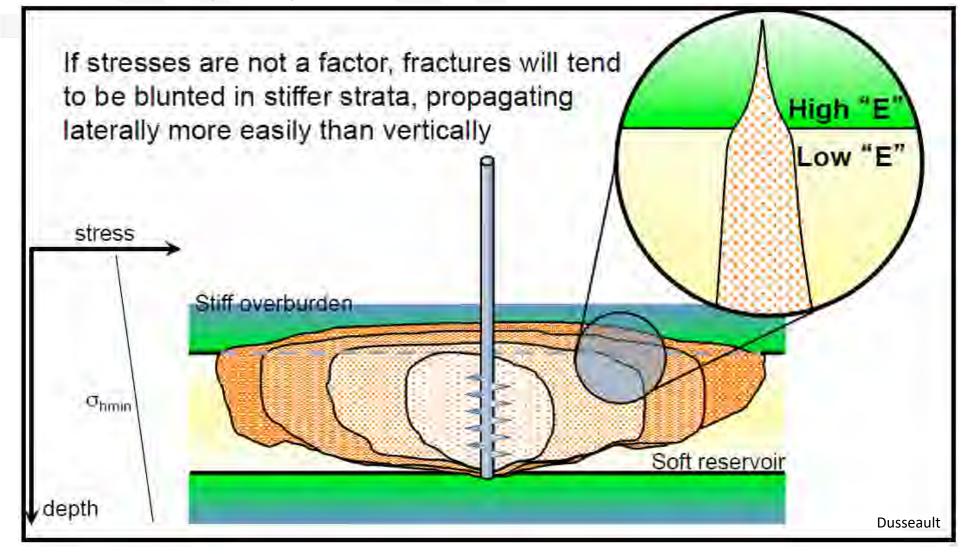
Strain



**GFZ** 



# Rock properties - mechanical







# **Key Components for EGS**



Rock properties Varying rock Material Properties (E, v)

Fracture networks

Varying fracture geometry, frequency, and interactions

**Stress** 

The fracture propagation is calculated using the non-local damage approach, combined with a cohesive-zone model



MATERIAL MECHANICAL PROPERTIES

CRACK OPENING BEHAVIOR





# Thank you very much for your attention









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TUDelft

